

DISCUSSION

Phillips Petroleum Company's No. 17 E. Coop, Osage County, Oklahoma, was cored for the purpose of determining the connate water saturation of the Burbank sand.

Cable tools were used in the coring of this well. Precautions were taken to insure recovery of a core which had been subjected only to a very minimum of water contamination and would as nearly represent formation connate water conditions as this method of coring would permit. A drilling fluid consisting of oil and a compound known by the trade name "Mulsor" was used in an effort to avoid or reduce contamination of the core by drilling water.

The drilling fluid was used in the following manner: First; to condition the hole and remove any water which may have been present, 20 gallons of fluid (80% oil and 10% Mulsor) was run into the hole with the bailer, agitated, and then bailed out. The water left in the hole after drilling the plug was emulsified with the oil by this treatment and then removed by three trips of the bailer. Second; for coring, 20 gallons of the fluid was mixed and run into the hole. The formation was then cored with a 4-1/2 inch Baker Cable tool core barrel employing 36 inch stroke with 24 strokes per minute. After pulling the core barrel, the hole was reamed down and the fluid bailed therefrom. Samples of the fluid recovered in the bailer consisted of an emulsion containing an appreciable amount of suspended sand cuttings. At no time during the coring operation was there any evidence of free water being bailed from the well.

This drilling fluid was used in the above described manner while coring from 3991 to 3019 feet.

The core from 3019 to 3029.5 feet was cut using oil alone as the drilling fluid. However, the drilling crew reported that effects from the Mulsor were noticed over the entire section.

From the standpoint of providing a method for assuring an uncontaminated core, results obtained from analysis of the cores, indicate that the method has promising possibilities. Insofar, however, as the recovery and condition of the core was concerned further improvements in obtaining larger biscuits of core are necessary. All of the core from the section of soft sand in the top of the formation was very badly broken. Only a few very thin biscuits and fragments of biscuits were obtained from this section, the greater part of the recovery consisting of unconsolidated sand. The biscuits from the firm sand in the bottom of the formation were of much more satisfactory size for analytical purposes than those obtained from the top of the formation.

Results from the analysis show that the formation consists of two sections of sandstone distinctly different in characteristics from each other. The upper section down to approximately 3019 feet consisted of soft, highly permeable sandstone with high porosity. The lower section, however, consisted of firm to hard sandstone with permeability considerably lower than that in the upper section and with porosity averaging from 15 to 16 percent.

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DISCUSSION

Total liquid saturation was found to be high throughout the entire core, averaging about 94 per cent of the pore space in the highly permeable section and about 90 per cent in the less permeable section. In the highly permeable sections, both water and oil saturations are higher than actual reservoir conditions due to infiltration of the emulsified drilling fluid. The infiltration of drilling fluid was greatest in the gas bearing section from 2991 to 3002 feet due to the lower liquid saturation in this part of the reservoir. The indicated connate water saturation in this gas bearing section is from 25 to 35 per cent of the pore space. Due to the small size of the recovered biscuits of core, it was necessary to use a sample composed of four to eight biscuits for each of the saturation determinations. The saturation tests were made on these consolidated biscuits of core, which were later also used for permeability and chloride determinations, the largest biscuit being used for the permeability test. Due to the small size of the biscuits, the infiltration of drilling fluid was greater than would be encountered if larger biscuits of core could be recovered.

The permeability-connate water saturation relation for the core data is presented in Figure 1. The solid line in the figure represents the uncontaminated samples. Less weight is given to some of the higher and intermediate permeability ranges due to these samples being affected by natural segregation and capillarity effects. The dashed curve gives weight to contaminated samples and represents minimum possible values for the connate water saturation. The solid line is considered to be the more reliable data in view of information available at this time.

CHW

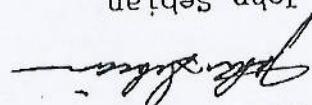
CORING RECORD

<u>Depth</u>		<u>Recovered</u>	
<u>From</u>	<u>To</u>	<u>Feet</u>	<u>Remarks</u>
2191.	2195.	4.	Very badly broken sandstone and unconsolidated sand.
2195.	3001	8.5	Upper 2-1/2 feet of recovery, unconsolidated sand believed to be cavings. Remainder of recovery consisted of unconsolidated sand and badly broken sandstone.
3001	3007	4.5	Badly broken biscuits of soft sandstone and unconsolidated sand.
3007.	3013.	6.	Badly broken biscuits of soft sandstone and unconsolidated sand.
3013	3019	4.	Badly broken biscuits of soft sandstone and unconsolidated sand.
3019	3024.5	4.5	Small biscuits of firm sandstone
3024.5	3029.5	3.	Small biscuits of firm sandstone.
3029.5 1901.5	3034 1906.0		Drilled sand (a small amount of water in bottom bailer)
3034. 1906.0	3034.5 1906.5		Drilled shale.

CLB
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JS/Ym

Laboratory Supervisor
John Seblian



CORE LABORATORIES
Very truly yours,

We trust these data will be useful in the evaluation of your property and thank you for the opportunity of serving you.

Core analysis data is presented in tabular and graphical form for our convenience. A porosity vs. permeability plot was prepared for statistical evaluation. Core analysis data is contained on a 3 1/2 inch computer diskette. Digital core photographs are contained on a CD.

The subject well was cored using diamond coring equipment and fresh mud to obtain 4 inch diameter cores from 3000 to 3035 feet and 3060 to 3071.4 feet from the Burbank Sand formation.

Gentlemen:

File No.: 57181-19029
Subject: Core Analysis Unit 39-28
North Burbank Field
Burbank, Oklahoma
Osage County, Oklahoma

CALUMET OIL COMPANY
2455 EAST 51st
Tulsa, Oklahoma 74105

December 20, 2005

Petroleum Services Division
2001 Commerce
Midland, Texas 79703
Tel: (432) 694-7761
Fax: (432) 694-3191
www.corelab.com



The cores were preserved at the wellsite in plastic bags and transported to Midland via motor freight by Stimp-Lab personnel. A Core Gamma Log was recorded for downhole E-Log correlation.

The core was taken from selected intervals and preserved in coresecal. The shale samples were wrapped in saran and foil. Coresecal was made on selected intervals recorded on full diameter samples. Plung samples taken were determined using a Dean Stark/ gas solvent extraction method.

Fluid removal and saturations were determined using a Dean Stark/

The core was photographed under ultraviolet light.

The cores were transported to Midland via motor freight by Stimp-Lab personnel.

Core analysis was made on selected intervals recorded on full diameter samples. Plung samples taken were determined using a Dean Stark/ gas solvent extraction method.

Full diameter porosity was determined by direct pore volume measurement using Boyle's Law helium expansion. Bulk volume was measured by Archimedes principle using Boyle's Law helium expansion. Bulk volume and grain volume measurements.

$$\text{Grain Density} = \frac{\text{Dry Weight}}{\text{Bulk Vol. - Pore Vol.}}$$

Plung direct grain volume measurement was made using Boyle's Law helium expansion. Bulk volume was measured by Archimedes principle on samples after cleaning. Porosity was calculated using bulk volume and grain volume measurements.

$$\text{Porosity} = \frac{\text{Bulk Vol. - Grain Vol.}}{\text{Bulk Vol.}} \times 100$$

Steady State At Permeability was measured in two horizontal directions and vertically while the core was coated in a Hassler rubber sleeve. The core was boxed after analysis.

The core will remain at our Midland Facility (thirty days free of charge) as we await further disposition instructions.

CORE LABORATORIES

Company : CALUMET OIL COMPANY
 Well : NORTH BURBANK UNIT 39-28
 Location : NW/4 SEC 23, T-27-N, R-5-E
 Co., State : OSAGE, OKLAHOMA

CORE ANALYSIS RESULTS

Field : BURBANK FIELD
 Formation : BURBANK SAND
 Coring Fluid : FRESH WATER MUD
 Elevation : 1138' KB

File No.: 57181-19029
 Date : 12/13/05
 API No. :
 Analysts: SEBIAN

SAMPLE NUMBER	DEPTH ft	PERMEABILITY		POROSITY (%)	SATURATION		GRAIN DENSITY gm/cc	DESCRIPTION
		(MAXIMUM) Kair	(90 DEG) VERTICAL Kair		(PORE VOLUME) OIL %	WATER %		
CORE NO. 1 3000.0-3035.0 CUT 35' REC 35'								
1	3000.0 - 01.0	1548.	1404.	914.	28.0	25.6	51.4	2.66 Sd. gry. med-f gr. 95% yel flu
2	3001.0 - 02.0	764.	681.	274.	25.9	28.3	53.9	2.66 Sd. gry. med-f gr. 95% yel flu
3	3002.0 - 03.0	647.	547.	317.	25.8	29.8	61.7	2.70 Sd. gry. med-f gr. 95% yel flu
4	3003.0 - 04.0	420.	418.	114.	24.3	29.5	61.0	2.68 Sd. gry. med-f gr. 95% yel flu
5	3004.0 - 05.0	319.	304.	93.0	23.1	28.2	53.0	2.67 Sd. gry. f-med gr. 95% yel flu
5	3005.0 - 06.0	129.	126.	10.5	19.8	21.1	74.0	2.66 Sd. gry. f-med gr. 95% yel flu
7	3006.0 - 07.0	69.6	69.1	15.6	18.7	19.0	72.4	2.68 Sd. gry. f-med gr. 95% yel flu
8	3007.0 - 08.0	60.2	59.8	7.89	18.0	18.4	69.9	2.68 Sd. gry. f-vf gr. 95% yel flu
9	3008.0 - 09.0	210.	207.	21.7	19.3	16.0	75.5	2.67 Sd. gry. f-vf gr. 95% yel flu
10	3009.0 - 10.0	358.	355.	348.	22.8	16.3	58.6	2.67 Sd. gry. med-f gr. 60% dull gld flu
11	3010.0 - 11.0	442.	420.	358.	23.8	17.7	72.1	2.67 Sd. gry. med-f gr. 50% dull gld flu
12	3011.0 - 12.0	443.	424.	23.6	19.2	71.5	2.66 Sd. gry. med-f gr. 50% dull gld flu	
*	3012.0 - 13.0	0.07	0.07	8.9	13.5	81.0	2.75 Sd. gry. vf-slt gr. 40% v/pale yel flu	
*	3013.0 - 14.0	0.39	0.39	10.0	17.1	76.1	2.71 Sd. gry. vf-slt gr. 60% v/pale yel flu	
*	3014.0 - 15.0	0.04	0.04	6.4	13.7	85.9	2.75 Sd. gry. vf-slt gr. trx v/pale yel flu	
*	3015.0 - 16.0	462.	462.	27.0	32.2	60.3	2.69 Sd. gry. med-f gr. 100% yel flu	
17	3016.0 - 17.0	1303.	1259.	28.9	31.1	66.9	2.63 Sd. gry. med-f gr. 90% yel flu	
18	3017.0 - 18.0	783.	696.	27.9	26.2	70.3	2.66 Sd. gry. med-f gr. 80% yel flu	
19	3018.0 - 19.0	688.	681.	113.	28.0	29.5	68.0	2.66 Sd. gry. f-med gr. 90% yel flu
20	3019.0 - 20.0	742.	734.	28.5	26.7	59.7	2.67 Sd. gry. f-med gr. 90% yel flu	
21	3020.0 - 21.0	838.	829.	433.	27.6	26.2	72.5	2.62 Sd. gry. f-med gr. 95% yel flu
22	3021.0 - 22.0	677.	665.	337.	27.5	21.2	74.1	2.63 Sd. gry. f-med gr. 95% yel flu
23	3022.0 - 23.0	688.	675.	451.	27.7	20.2	77.2	2.65 Sd. gry. f-med gr. 90% yel flu
24	3023.0 - 24.0	471.	468.	72.8	25.6	21.9	75.7	2.67 Sd. gry. med-f gr. 75% yel flu
25	3024.0 - 25.0	554.	549.	237.	26.3	16.8	80.2	2.66 Sd. gry. med-f gr. 50% dull gld flu

Company : CALUMET OIL COMPANY
Well : NORTH BURBANK UNIT 39-28

C O R E A N A L Y S I S R E S U L T S

Field : BURBANK FIELD
Formation : BURBANK SAND

File No.: 57181-19029
Date : 12/13/05

C O R E L A B O R A T O R I E S

SAMPLE NUMBER	DEPTH ft	PERMEABILITY			POROSITY (%)	SATURATION (%)	GRAIN DENSITY gm/cc	DESCRIPTION
		(MAXIMUM) Kair md	(90 DEG) Kair md	(VERTICAL) Kair md				
26	3025.0 - 26.0	499.	474.	199.	26.1	17.5	77.0	2.67 Sd. gry. med-f gr. 50% dull gld flu
27	3025.0 - 27.0	181.	179.	147.	26.5	21.7	72.6	2.67 Sd. gry. med-vf gr. 80% yel flu
28	3027.0 - 28.0	426.	406.	95.0	26.0	18.0	76.6	2.68 Sd. gry. f-med gr. 80% yel flu
29	3028.0 - 29.0	432.	413.	277.	25.3	16.3	78.3	2.67 Sd. gry. f-med gr. 80% yel flu
30	3029.0 - 30.0	241.	234.	39.4	22.5	15.6	70.9	2.68 Sd. gry. med-vf gr. 80% yel flu
- 31	3030.0 - 31.0	376.	370.	402.	25.7	14.9	74.8	2.67 Sd. gry. med-vf gr. 80% dull gld flu
32	3031.0 - 32.0	305.	292.	24.4	10.5	80.7	2.65 Sd. dk gry. med-vf gr. 20% dull gld flu	
33	3032.0 - 33.0	177.	175.	69.5	21.8	13.2	80.2	2.66 Sd. dk gry. med-vf gr. 20% dull gld flu
34	3033.0 - 34.0	107.	102.	9.50	18.4	11.9	73.1	2.68 Sd. dk gry. f-vf gr. 70% yel flu
35	3034.0 - 35.0	68.0	52.2	44.6	17.5	12.5	59.9	2.68 Sd. dk gry. f-vf gr. 85% yel flu

DRILLED INTERVAL 3035-3060

CORE NO. 2 3060.0-3071.4 CUT 11.4' REC 11.4'

*	36	3060.0 - 61.0	2.84	13.9	12.6	47.1	2.63	Sd. dk gry. vf-f gr. 0% flu gd cut
*	37	3061.0 - 62.0	1.71	11.2	10.5	53.7	2.67	Sd. dk gry. vf-f gr. 0% flu gd cut
*	38	3062.0 - 63.0	1.39	1.36	11.1	51.3	2.64	Sd. dk gry. vf-f gr. tr% yel flu gd cut
*	39	3063.0 - 64.0	8.55	8.08	4.80	14.0	4.9	43.1
*	40	3064.0 - 65.0	7.37	6.22	3.98	13.7	4.3	2.63 Sd. dk gry. med-vf gr. tr% yel flu gd cut
*	41	3065.0 - 66.0	0.81	0.74	0.28	11.3	16.6	44.9
*	42	3066.0 - 71.4				38.2	2.63	Sd. dk gry. med-vf gr. 10% dull gld flu
								No Analysis, Shale, blk

* INDICATES PLUG ANALYSIS

Chaparral Area permit pr18

Oilfield Research Laboratories

GENERAL INFORMATION & SUMMARY

Company	Phillips Petroleum Co.	Lease	N.B.U.	Well No.	9-W26
Location	NW $\frac{1}{4}$				
Section 11	Twp. 27N	Rge. 5E	County	Osage	State Oklahoma
Name of Sand					Burbank
Top of Core					2976.0
Bottom of Core					3024.0
Top of Sand	(Received)				2976.0
Bottom of Sand	(Received)				3024.0
Total Feet of Permeable Sand					45.0
Total Feet of Floodable Sand					
Distribution of Permeable Sand:					
Permeability Range Millidarcys		Feet	Cum. Ft.		
0 - 1	16.0	16.0			
1 - 20	4.0	20.0			
20 - 100	6.0	26.0			
100 - 500	15.0	41.0			
500 & above	4.0	45.0			
Average Permeability Millidarcys					154.2
Average Percent Porosity					19.8
Average Percent Oil Saturation					
Average Percent Water Saturation					
Average Oil Content, Bbls./A. Ft.					
Total Oil Content, Bbls./Acre					
Average Percent Oil Recovery by Laboratory Flooding Tests					
Average Oil Recovery by Laboratory Flooding Tests, Bbls./A. Ft.					
Total Oil Recovery by Laboratory Flooding Tests, Bbls./Acre					
Total Calculated Oil Recovery, Bbls./Acre					
Packer Setting, Feet					
Viscosity, Centipoises @					
A. P. I. Gravity, degrees @ 60 °F					
Elevation, Feet					

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Company Phillips Petroleum Co. Lease N.B.U. Well No. 9-W26Depth Interval, Description
Feet

2976.0 - 3000.0 - Brown sandstone.

3000.0 - 3024.0 ~ Dark carbonaceous sandstone.

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RESULTS OF PERMEABILITY AND POROSITY TESTS
TABLE I A

Company Phillips Petroleum Co. Lease N.B.U. Well No. 9-W26

Sample No.	Depth Feet	Permeability Millidareys	Feet of Core		Permeability Capacity Ft. x Md.	Percent Porosity
			Ft.	Cum. Ft.		
1	2976.1	247.	1.0	1.0	247.00	28.4
2	2977.1	415.	1.0	2.0	415.00	29.1
3	2978.1	130.	1.0	3.0	130.00	27.5
4	2979.1	153.	1.0	4.0	153.00	27.1
5	2980.1	644.	1.0	5.0	644.00	29.4
6	2981.1	436.	1.0	6.0	436.00	28.5
7	2982.1	122.	1.0	7.0	122.00	23.2
8	2983.1	68.	1.0	8.0	68.00	21.7
9	2984.1	44.	1.0	9.0	44.00	20.0
10	2985.1	20.	1.0	10.0	20.00	19.7
11	2986.1	226.	1.0	11.0	226.00	24.6
12	2987.1	143.	1.0	12.0	143.00	23.2
13	2988.1	61.	1.0	13.0	61.00	20.4
14	2989.1	60.	1.0	14.0	60.00	21.8
15	2990.1	314.	1.0	15.0	314.00	27.4
16	2991.1	399.	1.0	16.0	399.00	27.8
17	2992.1	384.	1.0	17.0	384.00	28.1
18	2993.1	319.	1.0	18.0	319.00	27.0
19	2994.1	436.	1.0	19.0	436.00	27.7
20	2995.1	599.	1.0	20.0	599.00	28.4
21	2996.1	556.	1.0	21.0	556.00	29.5
22	2997.1	298.	1.0	22.0	298.00	28.2
23	2998.1	509.	1.0	23.0	509.00	27.8
24	2999.1	322.	1.0	24.0	322.00	26.0
25	3000.1	0.70	1.0	25.0	0.70	11.0
26	3001.1	4.5	1.0	26.0	4.50	12.9
27	3002.1	27.	1.0	27.0	27.00	19.0
28	3003.1	0.34	1.0	28.0	0.34	10.3
29	3004.1	0.29	1.0	29.0	0.29	9.9
30	3005.1	Imp.	-	-	-	-
31	3006.1	0.24	1.0	30.0	0.24	8.6
32	3007.1	0.35	1.0	31.0	0.35	11.7
33	3008.1	0.93	1.0	32.0	0.93	13.1
34	3009.1	0.25	1.0	33.0	0.25	11.0
35	3010.1	0.30	1.0	34.0	0.30	12.2
36	3011.1	0.26	1.0	35.0	0.26	12.2
37	3012.1	0.36	1.0	36.0	0.36	12.9
38	3013.1	0.22	1.0	37.0	0.22	11.1
39	3014.1	0.21	1.0	38.0	0.21	10.9
40	3015.1	Imp.	-	-	-	-
41	3016.1	1.5	1.0	39.0	1.50	15.1
42	3017.1	2.0	1.0	40.0	2.00	18.0
43	3018.1	0.25	1.0	41.0	0.25	8.2

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RESULTS OF PERMEABILITY AND POROSITY TESTS
TABLE I A

Company Phillips Petroleum Co. Lease N.B.U. Well No. 9-W26

Sample No.	Depth Feet	Permeability Millidarcys	Feet of Core		Permeability Capacity Ft. x Md.	Percent Porosity
			Ft.	Cum. Ft.		
44	3019.1	Imp.	-	-	-	-
45	3020.1	0.85	1.0	42.0	0.85	15.7
46	3021.1	1.8	1.0	43.0	1.80	15.5
47	3022.1	0.38	1.0	44.0	0.38	13.7
48	3023.1	0.26	1.0	45.0	0.26	13.0

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SUMMARY OF PERMEABILITY & POROSITY TESTS

TABLE II A

Company	Phillips Petroleum Co.	Lease	N.B.U.	Well No
Depth Interval Feet	Feet of Core Analyzed	Average Air Permeability, Millidarcys	Average Effective Permeability, Millidarcys	Permeability Capacity Ft. x M.d.
2976.0 - 3000.0	24.0	288.0		6,905.00
3000.0 - 3024.0	21.0	2.0		42.99
2976.0 - 3024.0	45.0	154.2		6,947.99
				19.8

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GENERAL INFORMATION & SUMMARY

Company Phillips Petroleum Co. Lease N.B.U. Well No. 14-W22
Location SE $\frac{1}{4}$

Section 10 Twp 27N Rge 5E County Osage State Oklahoma

Top of Case 2995-0

Bottom of Core - - - - - 3045.0

Total Feet of Floodable Sand -

Distribution of Permeable Sand: West Coast, U.S.A.

<u>Immidarys</u>		
0 - 50	18.0	18.0
50 - 200	6.0	24.0
200 - 500	7.0	31.0
500 - 700	7.0	38.0
700 - 900	6.0	44.0
900 & above	6.0	50.0

Average Permeability Millidarcys - - - - - 389.0

Average Percent Oil Saturation - - - - - - - - - - - - -

Average Percent Water Saturation - - - - - - - - - - - - -

Average Oil Content, Bbls./A. Ft. - - - - - - - - - - - - -

Total Oil Content, Bbls./Acre - - - - - - - - - - - - - - -

Average Percent Oil Recovery by Laboratory Flooding Tests - - - - -

Average Oil Recovery by Laboratory Flooding Tests, Bbls./A. Ft. - - - - -

Total Oil Recovery by Laboratory Flooding Tests, Bbls./Acre - - - - -

Total Calculated Oil Recovery, Bbls./Acre - - - - - - - - - - -

Packer Setting, Feet -

Viscosity, Centipoises @ -

A. P. I. Gravity, degrees @ 60° F - - - - - - - - - - - - - - -

OILFIELD RESEARCH LABORATORIES

-LOG-

Company Phillips Petroleum Co. Lease N.B.U. Well No. 14-W22

Depth Interval, Description
Feet

2995.0 - 3025.0 - Fine grained, light brown sandstone.

3025.0 - 3045.0 - Brown, fine grained sandstone.

Oilfield Research Laboratories
RESULTS OF PERMEABILITY AND POROSITY TESTS
TABLE I A

Company Phillips Petroleum Co. Lease N.B.U. Well No. 14-W22

Sample No.	Depth Feet	Permeability Millidarcys	Feet of Core		Permeability Capacity Ft. x Md.	Percent Porosity
			Ft.	Cum. Ft.		
1	2995.5	967.	1.0	1.0	967.00	28.7
2	2996.5	533.	1.0	2.0	533.00	26.2
3	2997.5	146.	1.0	3.0	146.00	24.4
4	2998.5	1503.	1.0	4.0	1503.00	31.0
5	2999.5	125.	1.0	5.0	125.00	25.3
6	3000.5	458.	1.0	6.0	458.00	27.9
7	3001.5	46.	1.0	7.0	46.00	19.2
8	3002.5	148.	1.0	8.0	148.00	23.4
9	3003.5	1562.	1.0	9.0	1562.00	28.2
10	3004.5	81.	1.0	10.0	81.00	21.8
11	3005.5	321.	1.0	11.0	321.00	26.8
12	3006.5	829.	1.0	12.0	829.00	25.6
13	3007.5	956.	1.0	13.0	956.00	28.7
14	3008.5	713.	1.0	14.0	713.00	29.8
15	3009.5	1015.	1.0	15.0	1015.00	30.1
16	3010.5	1112.	1.0	16.0	1112.00	30.4
17	3011.5	581.	1.0	17.0	581.00	25.8
18	3012.5	788.	1.0	18.0	788.00	30.1
19	3013.5	572.	1.0	19.0	572.00	28.4
20	3014.5	581.	1.0	20.0	581.00	29.2
21	3015.5	502.	1.0	21.0	502.00	29.0
22	3016.5	542.	1.0	22.0	542.00	28.2
23	3017.5	553.	1.0	23.0	553.00	28.4
24	3018.5	738.	1.0	24.0	738.00	29.8
25	3019.5	873.	1.0	25.0	873.00	30.0
26	3020.5	738.	1.0	26.0	738.00	29.0
27	3021.5	492.	1.0	27.0	492.00	28.0
28	3022.5	324.	1.0	28.0	324.00	29.2
29	3023.5	365.	1.0	29.0	365.00	28.9
30	3024.5	472.	1.0	30.0	472.00	27.8
31	3025.5	266.	1.0	31.0	266.00	27.1
32	3026.5	100.	1.0	32.0	100.00	22.6
33	3027.5	59.	1.0	33.0	59.00	20.4
34	3028.5	36.	1.0	34.0	36.00	19.0
35	3029.5	10.	1.0	35.0	10.00	19.1
36	3030.5	33.	1.0	36.0	33.00	18.2
37	3031.5	36.	1.0	37.0	36.00	18.7
38	3032.5	19.	1.0	38.0	19.00	18.4
39	3033.5	28.	1.0	39.0	28.00	18.5
40	3034.5	24.	1.0	40.0	24.00	18.7
41	3035.5	26.	1.0	41.0	26.00	18.9
42	3036.5	15.	1.0	42.0	15.00	17.5
43	3037.5	20.	1.0	43.0	20.00	18.8

Oilfield Research Laboratories
RESULTS OF PERMEABILITY AND POROSITY TESTS
TABLE I A

Company Phillips Petroleum Co. Lease N.B.U. Well No. 14-W22

Sample No.	Depth Feet	Permeability Millidarcys	Feet of Core		Permeability Capacity Ft. x Md.	Percent Porosity
			Ft.	Cum. Ft.		
44	3038.5	8.1	1.0	44.0	8.10	18.0
45	3039.5	8.3	1.0	45.0	8.30	17.2
46	3040.5	29.	1.0	46.0	29.00	17.6
47	3041.5	20.	1.0	47.0	20.00	17.7
48	3042.5	18.	1.0	48.0	18.00	17.5
49	3043.5	21.	1.0	49.0	21.00	17.5
50	3044.5	20.	1.0	50.0	20.00	17.4

Oilfield Research Laboratories

SUMMARY OF PERMEABILITY & POROSITY TESTS

TABLE II A

Company	Phillips Petroleum Co.	Lease	N.B.U.	Well No. 14-W22
Depth Interval, Feet	Feet of Core Analyzed	Average Air Permeability, Millidarcys	Average Effective Permeability, Millidarcys	Permeability Capacity Ft. x Mi.
2995.0 - 3011.0	16.0	658.0	-	10,515.00
3011.0 - 3027.0	16.0	530.0	-	8,487.00
3027.0 - 3045.0	18.0	23.9	-	430.40
2995.0 - 3045.0	50.0	389.0	-	19,432.40

✓
✓
AFE No. P-3399

PHILLIPS PETROLEUM COMPANY
EXPLORATION AND PRODUCTION DEPARTMENT
Laboratory Reservoir Engineering

No. CA-29
Date Nov. 8, 1963

CORE ANALYSIS REPORT

NBU

Pool

Company Phillips Petroleum et al

Lease NBU 15

Description Sec. 11 - T27N - R5E

County Osage

^{Sec.} ^{Twp.} ^{Rge.}
420' FNL & 1285' FWL of SW/4

Well No. W-26

State Oklahoma

Dates of Coring: Started October 28, 1963

Completed October 29, 1963

Core Barrel

Size Core 2 3/4"

Elevations: Surface 1087.25'

Starting Point for Depth Measurements RKB 1094.75'

Depth Measurements by Drill pipe

Last Steel Line Measurements

Formation Cored: Name Burbank Sand

Top 2929'

Bottom

Purpose of Coring

Requested by Mr. Earl Griffin

Copies to Messrs.: M. J. Kaufman (r)

T. A. Matthews (12)

W. A. Roberts

R. W. O'Neill

J. W. Marx

F. W. Beghtel

J. F. Downie

COPY FOR

10/18

NBU 15 WELL N.W-26

CORE ANALYSIS.

Form 864-C 1-61

Sample Core No. No.	DEPTH IN FEET	PERMEABILITY		POROSITY		SATURATION		GRAIN		COMBUSTIBLE GAS		REMARKS
		MILLIDARCY'S	Per cent dicular	On Pore Sample	On Sat. Sample	Oil	Water	Total	DENSITY	Methane Plus	Propane Plus	
1	Cored	2933	2932	2932	2932	2981	Recover	50	100%	2.6.8		
2	2933	2934		280.	26.8					2.7.0		
3	2934	2935		135	25.0					2.7.3		
4	2935	2936		4.3	11.5					2.8.3		
5	2936	2937		108	35.9					3.6.8		
6	2937	2938		146	25.7					3.6.8		
7	2938	2939		210.	25.1					3.6.7		
8	2939	2940		780.	26.6					3.6.7		
9	2940	2941		122	25.4					3.6.8		
10	2941	2942		210.	35.9					3.6.8		
11	2942	2943		160.	26.2					3.6.7		
12	2943	2944		573	26.7					3.6.7		
13	2944	2945		491	27.3					3.6.8		
14	2945	2946		220.	25.0					3.6.8		
15	2946	2947		264	24.7					3.6.8		
16	2947	2948		791	26.7					3.6.8		
17	2948	2949		525	26.7					3.6.9		
18	2949	2950		64	26.0					2.7.0		
19	2950	2951		536	26.7					2.6.8		
20	2951	2952		177	26.1					2.6.9		
21	2952	2953		133	23.3					2.6.9		
22	2953	2954		119	24.6					2.6.9		
23	2954	2955		622	27.2					2.6.9		
24	2955	2956		675	27.6					2.6.8		
25	2956	2957		460	26.9					2.6.9		
26	2957	2958		89	21.7					2.6.8		
27	2958	2959		78	27.8					2.6.7		
28	2959	2960		760	27.5					2.6.8		
29	2960	2961		500	27.0					2.6.8		
30	2961	2962		808	27.4					2.6.8		
31	2962	2963		675	26.3					2.6.8		
32	2963	2964		945	27.6					2.6.8		
33	2964	2965		365	25.5					2.6.8		
34	2965	2966		735	26.7					2.6.8		
35	2966	2967		660	26.4					2.6.7		
36	2967	2968		329	23.0					2.6.8		
37	2968	2969		495	24.3					2.6.8		
38	2969	2970		616	34.8					3.7.0		

* Parts chloride per million parts of water from core.

Page No. 1

Date Nov. 8, 1963

Test Made By COSTELLO

Approved _____

ABU 15 WELL NO. W-26

Form 864-C 1-61

CORE ANALYSIS

Sample Core No. No.	DEPTH IN FEET		PERMEABILITY MILLIDARCY'S		POROSITY PER CENT		SATURATION PER CENT		GRAIN DENSITY	COMBUSTIBLE GAS	REMARKS
	From	To	Perpen- dicular	Parallel	On Sample	On Sample	Oil	Water Total			
39	1	2970	2971	4222	2.4/				2.66		
40	2971	2972	3681	23.2					2.65		
41	2972	2973	4651	23.5					2.65		
42	2973	2974	4651	23.0					2.63		
43	2974	2975	1901	20.3					2.63		
44	2975	2976	1801	24.4					2.65		
45	2976	2977	3321	22.5					2.65		
46	2977	2978	81.6	17.2					2.62		
47	2978	2979	5.1	11.3					2.57		
48	2979	2980	<.05	3.8					2.63		
49	2980	2981	13.7	14.5					2.65		
50	2981	2982	9.	10.8					2.61		

Approved _____

Test Made By _____

Cost & BuCE

* Parts chloride per million parts of water from core.

Date Nov. 8, 1963Page
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CORE ANALYSIS

Sample No.	Core No.	DEPTH, FEET		PERMEABILITY		SATURATION			COMBUSTIBLE GAS			REMARKS		
		FROM	TO	MILLIDARCY	Parallel Perpendic. ular	POROSITY Per Cent	Oil Per Cent	Water Per Cent	Total Per Cent	Chloro Formic Water P. P. N. P. ♦	METHANE PLUS	PROPANE PLUS	BUTANE PLUS	
1		3020.0	3020.5		959.	27.1								
2		3022.0	3022.5			781.	29.1							
3		3024.0	3024.5			83.3	21.0							
4		3026.0	3026.5			168.	23.2							
5		3028.0	3028.5			34.9	21.8							
6		3030.0	3030.5			56.7	19.5							
7		3032.0	3032.5			34.0	22.2							
8		3034.0	3034.5			503.	26.6							
9		3036.0	3036.5			323.	23.5							
10		3038.0	3038.5			382.	24.4							
11		3040.0	3040.5			74.1	25.7							
12		3042.0	3042.5			108.	11.4							
13		3044.0	3044.5			105.	22.8							
14		3046.0	3046.5			38.7	21.2							
15		3048.0	3048.5			1.1	11.5							
16		3050.0	3050.5			.02	5.7							
17		3052.0	3052.5			1.3	18.6							
18		3054.0	3054.5			161.	22.0							
19		3056.0	3056.5			183.	21.6							
20		3058.0	3058.5			104.	19.5							
21		3060.0	3060.5			76.2	19.5							
22		3062.0	3062.5			1.7	12.3							
23		3064.0	3064.5			8.0	14.9							
24		3066.0	3066.5			3.3	13.1							
25		3068.0	3068.5			1.5	10.1							
26		3070.0	3070.5			.9	10.7							
27		3072.0	3072.5			5.9	13.1							
28		3074.0	3074.5			3.6	11.8							
29		3076.0	3076.5			3.9	12.1							
30		3078.0	3078.5			2.7	11.3							
31		3080.0	3080.5			4.1	11.5							
32		3080.5	3081.0			1.7	11.2							

° Basis calculated per million pounds of water from core

